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DATA INTERFACE CIRCUITS FOR PSK MODULATORS FOR DATA TRANSMISSION FROM SPACE TO GROUND

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Comprehensible Electromagnetics for Comprehensive Engineering

Test Equipment

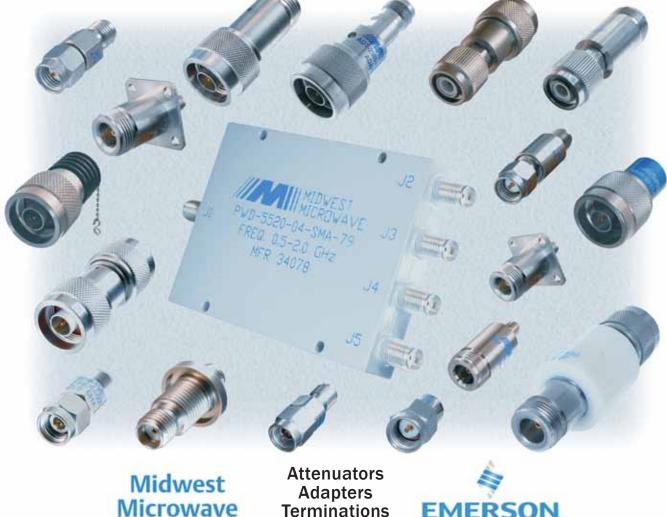
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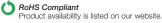
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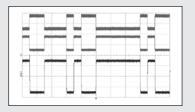
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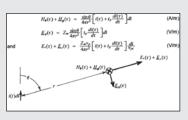
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Getting Connected in 2012

Scott L. Spencer **Publisher**



anuary 2012 marks the beginning of our 10th year as High Frequency Electronics magazine. Of the numerous topics we cover during a 12-month editorial cycle none is more popular than cables and connectors. This may be the case because most engineers must familiarize themselves with the nomenclature and performance characteristics of not only the numerous types of transmission lines available, but also with the host of connector families available.

In the 1980s I worked for Omni Spectra, a leading supplier of a variety of products including SMA connectors. We didn't call them SMAs; instead they were referred to as OSMs -- Omni Spectra Miniatures. Omni Spectra engineers knew that by not just meeting -- but exceeding -- the requirements of prevailing Mil-Spec, Mil-C-39012, the OSM would outperform the generic SMA every time. So, by design and via strict controls on machining and assembly operations, Omni Spectra was able to produce a superior connector that users preferred. By holding positions of the center conductor and dielectric in a tight tolerance position with respect to the connector reference plane, performance was improved to behave more like a continuous transmission line. Tighter manufacturing tolerances could sometimes lead to poor yields and delivery slippages, but these problems were soon overcome. The OSM brand name was synonymous with quality. Component designers knew that input and output VSWR requirements were more likely to be met with an OSM. Savvy system-level integrators knew that solid transmission line interconnects served to cut tuning time and rework costs.

The Connector Kings

If such statistics are even kept, it is likely that no one man ever purchased more microwave connectors than Mike Peacock. Mike recently retired from Raytheon in Goleta, Calif. He began purchasing connectors for Raytheon in 1962. Legendary Southern California microwave distributor C.W. "Chuck" Swift was the Omni Spectra distributor in California for much of Mike's career. Raytheon Goleta used boatloads of OSMs on phase-matched cables made from .141 semi rigid cable for use on their Surface Navy Electronic Warfare suites. The systems used large beam-forming lenses driven by miniature TWTs and semi-rigid cable was everywhere. All of it terminated with OSMs.

Chuck pilots a Beechcraft Bonanza that he purchased at the height of Omni Spectra's business success. The vanity tail numbers on the plane read "201 Whiskey Charlie." In what may be pure coincidence, 201 was the part

number Omni Spectra assigned to its largest selling connector--the OSM that terminates .141 semi-rigid.

Today there are numerous suppliers of precision SMA connectors and, to a large degree, they are a price-driven commodity. On the development front, smaller line sizes, more use of air dielectrics, improvements in cable performance, better durability, blind mating considerations, and color coding standards are the trends.

2012 Outlook

Many analysts believe that global GDP growth will slow in 2012 to around 3.2% with modest improvements in 2013. The U.S. could see domestic GDP grow as slow as 2% in 2012. There has been dialogue from that Washington the Super Committee impasse may trigger massive spending cuts to our defense programs. The Secretary of Defense recently warned that cutting \$1 trillion from the nation's defense spending over the next 10 years would gut almost every high-priority program. The F-35 Joint Strike Fighter, the Air Force's next generation bomber program, the Navy's SSBN-X submarine replacement program, the Navy's next generation Littoral Combat Ship, new satellite, surveillance and reconnaissance systems -- all could be affected. This would have a significant adverse impact on suppliers heavily invested in those programs and to their subcontractors and vendors. Another concern for 2012 is possible fallout from the unresolved European sovereign debt crisis which has the potential to put a heavy burden on the global financial system, slowing the growth of emerging economies.

On the other hand, the end of 2011 saw almost every major indicator of economic health moving in the right direction. The DJIA ended the year well above 12,000. Let's say Europe starts to stabilize and fastgrowing places like China, India, Indonesia, Brazil and Russia continue to grow at a faster pace than the U.S. If that scenario plays out and Washington comes up with a plan that addresses deficit reduction while continuing to invest in vital defense programs like the F-35, then economic opportunity will grow not only for this industry but also for the larger economy as a whole.

Upcoming

Don't forget DesignCon 2012. This year it is being held at the Santa Clara, Calif., Convention Center from January 30 through February 2, and is billed as the event "Where Chipheads Connect."



CONFERENCES

January 15 – 18, 2012

IEEE Radio and Wireless Symposium

12th Topical Meeting on Silicon Monolithic Integrated Circuits in RF Systems (SiRF)

2012 IEEE Topical Conference on Biomedical Wireless Technologies, Networks, and Sensing Systems (BioWireleSS)

2012 IEEE Topical Conference on Wireless Sensors and Sensor Networks (WiSNET)

2012 Topical Conference on Power Amplifiers for Wireless and Radio Applications (PAWR)

Santa Clara, Calif. Information: http://www.radiowirelessweek.org

February 6 – 8, 2012

Military Radar Summit Washington, D. C. Information: militaryradarsummit.com

March 5 – 7, 1012

IEEE International Workshop on Antenna Technology: Small Antennas and Unconventional Applications

Tucson, Ariz.

Information: http://www.cccmeetings.com/iwat2012.pdf

March 12 - 13, 2012

CS Europe Frankfurt, Germany Information: http://cseurope.net

April 1 – 4, 2012

IEEE Wireless Communications and Networking Conference

Paris, France Information: http://www.ieee-wcnc.org/2012

April 3 – 5, 2012

Microwave & RF Paris, France Information: http://www.microwave-rf.com/?lang=EN

April 3 – 5, 2012

Forum Radiocoms Paris, France Information: http://www.microwave-rf.com/

April 10 – 14, 2012

28th International Review of Progress in Applied Computational Electromagnetics

Columbus, Ohio Information: http://aces.ee.olemiss.edu

June 17 – 22, 2012

IMS 2012

Montreal, Canada Information: http//ims2012.org

August 6 – 9, 2012

NIWeek 2012 Austin, Tex. Information: http://www.niweek/

SHORT COURSES

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May 21 – 25, 2012, Burlington, Mass.

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MEETINGS & EVENTS

Power Conversion & Regulation Circuits for VLSI Systems

May 22 – 25, 2012, Burlington, Mass. Wireless/Computer Network Security

May 23 – 25, 2012, Burlington, Mass.

RF Fundamentals June 25 – 29, 2012, Web Classroom, WebEx

Company-Sponsored Training & Tools

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LabVIEW Core 1 Online http://sine.ni.com/tacs/app/fp/p/ap/ov/pg/1/ LabVIEW Core 2 Online http://sine.ni.com/tacs/app/fp/p/ap/ov/pg/1/ Object-Oriented Design and Programming in LabVIEW Online

http://sine.ni.com/tacs/app/fp/p/ap/ov/pg/1/

Agilent Technologies

Introduction to Agilent VEE Pro February 14 – 17, 2012, Las Vegas, Nev. http://www.home.agilent.com/agilent/eventDetail. jspx?cc=US&lc=eng&ckey=701878-14&nid=-34787.0.00&id=701878-14

RF and Microwave Fundamentals February 14 – 17, 2012, Las Vegas, Nev. http://www.home.agilent.com/agilent/eventDetail. jspx?cc=US&lc=eng&ckey=701878-14&nid=-34787.0.00&id=701878-14

Advanced Agilent VEE Pro June 19 – 22, 2012, Las Vegas, Nev. http://www.home.agilent.com/agilent/eventDetail. jspx?cc=US&lc=eng&ckey=701878-14&nid=-34787.0.00&id=701878-14

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CALL FOR PAPERS

2012 IEEE 13th Annual Wireless and Microwave Technology Conference (WAMICON)

April 16 – 17, 2012, Cocoa Beach, Fla. Abstract Deadline: January 9, 2012 Final Paper Deadline: February 13, 2012 http://ieee.org/web/callforpapers

2012 IEEE International Conference on Wireless Information Technology and Systems (ICWITS)

July 29 – August 3, 2012, Honolulu, Hawaii Abstract Deadline: April 1, 2012 http://ieee.org/web/callforpapers

2012 Workshop on Integrated Nonlinear Microwave and Millimetre –Wave Circuits

September 3 – 4, 2012, Dublin, Ireland Abstract Deadline: May 4, 2012 Final Paper Deadline: August 3, 2012 http://ieee.org/web/callforpapers

2012 IEEE International Conference on Ultra-Wideband (ICUWB2012)

September 17 – 20, 2012, Syracuse, N.Y. Abstract Deadline: March 9, 2012 Final Paper Deadline: June 15, 2012 http://ieee.org/web/callforpapers

2012 37th International Conference on Infrared, Millimeter, and Terahertz Waves

September 23 – 28, 2012, Wollongong, NSW, Australia Abstract Deadline: April 20, 2012 Final Paper Deadline: July 6, 2012 http://ieee.org/web/callforpapers

2012 IEEE 21st Conference on Electrical Performance of Electronic Packaging and Systems

October 21 – 24, 2012, Tempe, Ariz. Abstract Deadline: July 1, 2012 Final Paper Deadline: July 8, 2012 http://ieee.org/web/callforpapers

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IN THE NEWS

Business News

Analog Devices Inc. was named one of the world's most innovative companies, according to the Thomson Reuters 2011 Top 100 Global Innovator SM program. The program analyzes patent data and related metrics in a proprietary methodology to identify the organizations that lead the world in innovation activity. Analog Devices was one of 14 semiconductor and electronic component manufacturers named to the top 100, and the only analog company on the list of global innovators. "Analog Devices was built on the strength of our ability to differentiate our products, our signal processing technology and our approach to design collaboration and customer support. This is how we define innovation at ADI," said Robert McAdam, vice president, Core Products and Technologies Group, Analog Devices. The Thomson Reuters 2011 Top Global innovators program evaluates innovation performance according to companies that invent on a significant scale, work on developments that are acknowledged as innovative by others around the world, and whose inventions are globally protected due to their importance. The program's methodology is based on four principle criteria: patent approval success rate, global reach of patent portfolio, patent influence in literature citations and overall patent volume.

Micronetics, Inc. announced that it has been awarded an initial production order valued at approximately \$2.4 million from a leading precision antenna system manufacturer for the supply of high performance microwave subsystems. Each subsystem, which consists of a transceiver, on board computer, power supply, and a high power amplifier (HPA), will help satisfy the demanding need for a reliable, high-speed broadband satellite based connection into commercial and military aircraft for a broad range of uses. Hardware deliveries are targeted to commence in this fiscal year with a 6-month period of performance. David Robbins, Micronetics' CEO stated, "We are happy to have secured this initial contract. This product and design win reflects our latest in engineering expertise and we are optimistic that demand for this product will contribute to our growth. We targeted airborne high speed data links based on the strength and diversity of commercial and military applications, consistent with our strategy to leverage our strong technology capabilities and breadth of product offerings across multiple end markets."

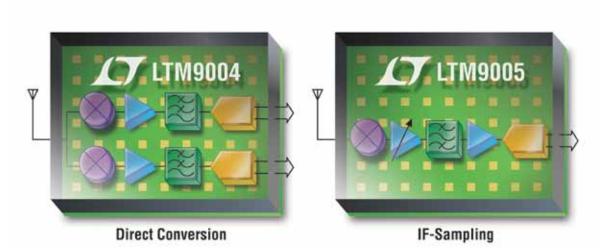
STMicroelectronics has been recognized as among the world's four best semiconductor companies in design, according to a report **from Gary Smith EDA**, a provider of market intelligence and advisory services for the global Electronic Design Automation (EDA), Electronic System Level (ESL) design, and related technology markets. In the report, founder and Chief Analyst Gary Smith, highlights ST's leadership in Electronic System Level (ESL) design, the depth of its expertise, and the contribution of its Computer-Aided Design (CAD) group. "ST has pioneered many of the tools and design methodologies presently used today. The design industry owes them their thanks for ST's design group's leadership in developing the ESL (Electronic System Level) methodology, said Gary Smith. Philippe Magarshack, Group Vice President of STMicroelectronics' Central CAD & Design Solutions Division, said, "Mr. Smith has extensive experience in assessing chip-design businesses, and his opinions are valued and recognized throughout the global semiconductor industry. The report findings further highlight ST's focus on design, which is a key source to providing our customers competitive advantage, and underpin ST's commitment to merging first-rate skills and facilities to deliver products with superior characteristics for our customers."

RF Micro Devices, Inc. announced that Huawei Technologies Corp., Ltd., a leading global information and communications technology (ICT) solutions provider, has honored RFMD with Huawei's 2011 "Best Supplier Award." The prestigious award was accepted by RFMD's president and CEO, Bob Bruggeworth, at an awards ceremony held earlier today in Shenzhen, China. Mr. Bruggeworth commented following the ceremony, "It is a distinct honor to receive this award from Huawei in recognition of RFMD's commitment to excellence in on-time product delivery, local customer support, and product and technology leadership. RFMD is proud to support Huawei across multiple product applications, including cellular handsets, smartphones, wireless infrastructure, and point-to-point cellular backhaul." Anders Karlborg, Vice President of Huawei Supply Chain Management, said, "RFMD is a strategic partner to Huawei whose dedication to customer service and support contribute directly to our success, especially in the areas of technology development and performance, field applications support, and product delivery."

Technology News

u-blox, the Swiss positioning and wireless chip and module company, and **Rohde & Schwarz (R&S)**, a leading supplier of test and measurement equipment, have successfully concluded a simulation of the Russian **GLONASS satellite navigation system**. The test, carried out with the R&S SMBV100A vec-

RF-to-Bits



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IN THE NEWS

tor signal generator and its GNSS simulation options, verified the u-blox proof-of-concept and the compatibility of u-blox receiver technology with the GLONASS transmission protocol. The GLONASS satellite system is Russia's answer to the US NAVSTAR GPS satellite positioning system. It will provide a high-accuracy positioning system with global coverage once completed. GLONASS will also be used in hybrid receivers around the world in conjunction with GPS to ensure improved coverage especially in dense cities and thus improve the location accuracy. "Our close cooperation with Rohde & Schwarz has proven to be a valuable and strategic asset, allowing us to develop advanced satellite receiver technology well before the actual satellites are available" said said Thomas Nigg, VP Product Marketing at u-blox. "u-blox, with its depth of expertise in GNSS technologies, has helped us to validate our satellite simulator technology," said Andreas Pauly, Head of R&D Signal Generators Baseband at Rohde & Schwarz. "Now we have enhanced our cutting-edge test equipment for GLONASS that simulates the protocol and physical layer."

People in the News

Texas Instruments Incorporated announced the election of three of its engineers to IEEE Fellow, a distinction reserved for select IEEE members whose extraordinary accomplishments are deemed fitting of this prestigious honor. TI's Ajith Amerasekera, director of Kilby Labs, Ahmad Bahai, Analog Chief Technology Officer, and Luigi Colombo, TI Fellow in the External Development and Manufacturing (EDM) group, received the IEEE's highest level of membership for their innovative contributions in the semiconductor industry. They join 19 other TI engineers who hold the prestigious title of IEEE Fellow. "Innovation is the foundation upon which TI's 80-plus year history is built," said Rich Templeton, chairman, president and CEO of Texas Instruments. "The election to IEEE Fellow is an extraordinary accomplishment, recognizing those who have driven significant innovations impacting our industry and the world we live in. We're fortunate to have some of the brightest minds working at TI." The IEEE Grade of Fellow is conferred by the IEEE Board of Directors upon a person with an outstanding record of accomplishments in any of the IEEE fields of interest. The total number selected in any one year cannot exceed one-tenth of one- percent of the total voting membership. IEEE Fellow is the highest grade of membership and is recognized by the technical community as a prestigious honor and an important career achievement. Three hundred and

twenty-one individuals have been elevated to IEEE Fellow for 2011.

Giga-tronics announced that **Robert Waldeck** has been named Vice President of Business Development for Switching Solutions. Mr. Waldeck has held positions as a Sales Representative and in Sales Management in



the T&M instrument industry during the past 15 years and prior to that worked in the Defense and Space industry. Mr. Waldeck spent over 16 years developing Automated Test Equipment for various branches of

the Armed Forces at a prominent Defense contractor. He holds a BSEE from NY Institute of Technology and an MBA from CW Post, Long Island University. "With the addition of Bob, Giga-tronics significantly strengthens its business of delivering high performance RF and Microwave signal switching solutions to its customers," said **Malcolm Levy**, Executive VP of Sales.



A new exhibit at the Computer History Museum in Mountain View, Calif., features work and artifacts from the life of Jim Williams, a towering figure in the world of engineering and one of the world's best analog circuit designers. A longtime employee of Linear Technology, Mr. Williams passed away in June 2011. According to the Museum, "The practice of designing analog circuits and systems is as much art as science. Real world signals vary continuously and can be complex and sometimes unpredictable. Analog engineers must combine technical knowledge with a great deal of experience and intuition in order to harness them. Analog designers often work under a master engineer, such as Jim Williams, for many years to learn the secrets of good analog design. This long apprenticeship gives them a special status among other engineers who consider analog design to be a mysterious process. Williams himself did not consider it a mystery." Information: computerhistory.org/highlights/analoglife/.

Low Power 16-Bit High Speed ADCs



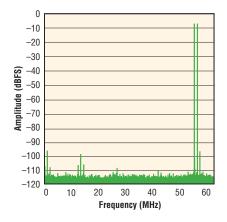
Flexible Digital Outputs: CMOS, DDR CMOS, DDR LVDS, Serial LVDS

Our lowest power 16-bit, 25Msps to 125Msps single and dual ADC families offer a choice of full-rate CMOS, DDR CMOS/LVDS or serial LVDS digital outputs with programmable timing, programmable LVDS current and optional LVDS termination. The ADCs feature Linear's digital output randomizer for reducing digital feedback. Designers can benefit from the choice of flexible interfaces to minimize pin count and ease routing to FPGAs.

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 - LTC2195: Serial LVDS
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- Optional Clock Duty Cycle Stabilizer
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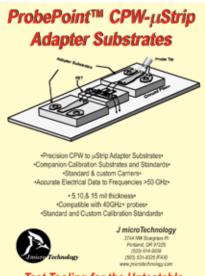
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tion test set for LTE. In addition, the E5515E wireless test set supports the latest TDSCDMA advancements such as TDHSDPA 2.8-Mb/sec IP data connections, TDHSUPA signaling and testmode connections, and TDSCDMA protocol logging.

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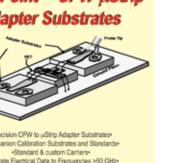
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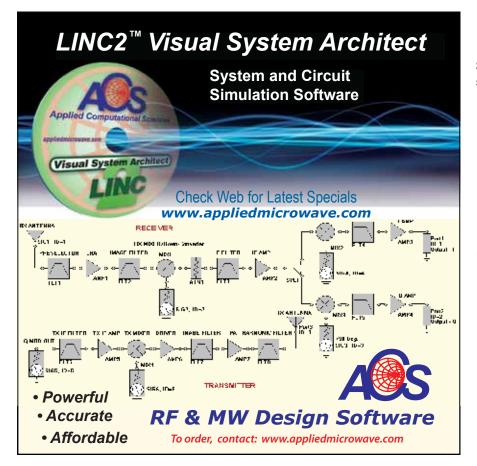
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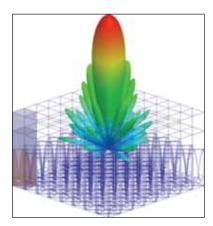
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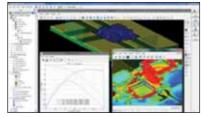
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efits such as simplifying the integration of new cores that can be reused across multiple designs. It provides a library of off-the-shelf IP cores and automates the creation and compilation of ISE projects in addition to simulation scripts. Stellar IP is available for free as part of the 4DSP Board Support Package targeting the 4DSP FMC and Virtex-6 FPGA product lines (http://www.4dsp.com/fmc, http:// www.4dsp.com/v6).

4DSP 4dsp.com



3-D Modeler

Agilent Technologies Inc. announced shipment of the latest release of its Electromagnetic Professional software, EMPro 2011.11. The updated 3-D modeling and simulation platform features enhancements to further speed and improve RF design and verification. EMPro is used to create 3-D models and analyze electrical performance of packages, connectors, antennas and other RF components. The EMPro 2011.11 release builds on advances made available in the 2011.07 release, introducing key improvements to the finite-element method simulator: • A fast FEM iterative solver that doubles the speed of simulations that include internal ports (which had already been doubled in the previous release). This continuous improvement reflects Agilent's ongoing commitment to fast-paced advancements in simulation technology. • A user-defined passive loads capability. This allows users to include ideal passive loads directly in an FEM simulation to represent matching circuits and surface-mount components. (The loads are defined in the EM setup environment, which consists of common series and parallel RLC network topologies. This capability enables accurate field visualization results and radiation patterns that take into account passive loads.) • A fast, twodimensional port solver that simplifies FEM simulation port setup. The solver allows users to quickly and easily determine the number of modes, as well as reference impedance and optimum impedance line placement.

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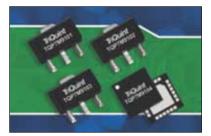
ICs



Bluetooth IC

Nordic Semiconductor announced that an enhanced revision of its nRF8001 Bluetooth 4.0 low energy Connectivity IC will further extend the current device's class-leading power-saving performance and benefit from an upgraded Bluetooth core software stack. The revision - which will be called the nRF8001 'Build D' and is already sampling to selected leading customers - is fully drop-in compatible (hardware and software) with the current Nordic nRF8001 (Build C) ensuring a smooth migration path for existing customers. The new power saving features and enhanced Bluetooth stack (see below) are easily accessible through an expanded Application Controller Interface (ACI) command set that can be used by extending existing application code. The nRF8001 Build D includes all Bluetooth core stack features required for the newly adopted Bluetooth low energy human interface device (HID) profile. This makes the nRF8001 an ideal solution for emerging Bluetooth low energy wireless PC peripherals and advanced navigational remotes for connected TV and set-top boxes (STB).

Nordic Semiconductor nordicsemi.com



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TriQuint Semiconductor, Inc. has released two new linear RF amplifier family members that lower power consumption while protecting mobile networks from disruption and service failures. Setting these amplifiers apart are patentpending integrated protection features that can guard against ESD and DC over-voltage electrical spikes. TriQuint also integrates RF over-drive protection to reduce the chance of damage from high signal levels often seen in systems employing digital pre-distortion linearization techniques commonly utilized in 3G/4G BTS network transceivers. The new 1 Watt TQP7M9103 and 2 Watt TQP7M9104 are ideal for 3G/4G wireless infrastructure applications including base transceiver stations, repeaters, boosters, remote radio heads, defense/aerospace and other wireless systems requiring high linearity and gain with low power consumption. The new devices help designers simplify RF connectivity through reduced bills of materials, increased efficiency and packaged design convenience.

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Data Interface Circuits for PSK Modulators For Data Transmission from Space to Ground

By Jolie. R and D.V. Ramana

In Indian Remote Sensing Satellites, payload data is transmitted from space to ground using a PSK modulator. The PSK modulator may be BPSK, QPSK or 8PSK depending on the volume of data to be transmitted. n Indian Remote Sensing Satellites, payload data is transmitted from space to ground using a PSK modulator. The PSK modulator may be BPSK, QPSK or 8PSK depending on the volume of data to be transmitted. Different data standards such as

TTL, RS-422 and LVDS can be used for transmission of payload data to the modulator onboard the satellite. An interface circuit is required to convert the received data to bipolar levels required for the modulator. This article discusses various interface circuits, hardware realization, and test results.

Introduction

A PSK modulator is used to modulate a high frequency carrier. The carrier frequency should be in the band allotted for data transmission (20 MHz in S-band and 375MHz in X-band), from space to ground. The PSK modulator used is either BPSK or QPSK, depending on the data throughput. In future, it is also envisaged to use an 8-PSK modulator for higher data rate transmission. The payload data from an on-board satellite camera is processed and fed to the modulator. Various logic interfaces such as TTL, RS422 and LVDS can be used. The payload data needs to be converted from the chosen logic level to bipolar levels required to switch the diodes in the modulator.

The data interface circuit for the modulator needs to be designed carefully since the data levels control all the characteristics of the modulator. The main characteristics of a modulator include carrier suppression, phase imbalance and amplitude imbalance. Each characteristic of the modulator is dependent on its drive levels, i.e., the level of data input. The interface circuit can be tuned to get optimized modulator performance. The number of streams of data depends on the PSK modulation scheme used.

In this paper, various modulator data interface circuits such as TTL, RS-422 and LVDS, which are used in Indian Remote Sensing Satellites, are discussed.

Transistor-Transistor Logic (TTL) Interface Circuit

For many years, TTL logic has been used for data transfer between the on-board data processing circuits and the RF modulator. The TTL logic family is relatively slow compared to many of the fast switching logic families available today. However, it was used recently in satellite applications where the data rate is 52.5 Mbps per stream. The total data rate transmitted using QPSK modulation is 105Mbps.

A TTL driver circuit for the modulator, designed and realized for space applications, is shown in Fig.1. The TTL logic levels are 0V and 5V. Initially, the data transmission rate was 5.2Mbps and TTL interface was used for a BPSK modulator. As the volume of payload data increased, the data transmission rates using TTL have been set to as high as 52.5Mbps per channel and QPSK modulation is used.

Three RG316/U cables (for I-data, Q-data and Clock) are used for data transmission



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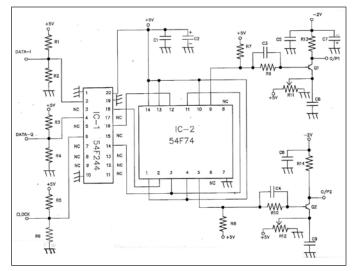


Figure 1 • TTL driver circuit

between the data processing package and the RF modulator package. The data processing and modulator packages are mounted at different locations on the satellite panels and the length of the cables carrying 52.5Mbps data is of the order of 3.9m each. As the data passes through lengthy cables, it is observed that the data quality degrades in terms of rise/fall time and duty cycle. This is due to parasitic capacitance in the long length of cables. The data quality is regenerated by passing through a buffer.

The TTL driver circuit consists of a buffer (54F244), D-flip flop (54F74), switching transistors (NE 88908) and passive components. The high speed buffer (54F244) is used at both the transmitting and receiving ends of the data transmission cables. The buffered I-data, Q-data and Clock are fed to a latch 54F74 IC. Here, the clock is used to synchronize the two data streams so that both appear at the modulator at the same time. The latched I and Q data are fed to switching transistors to convert them to bipolar levels required for biasing the PIN diodes in the reflection type modulator. The potentiometers in the circuit are finetuned to achieve the appropriate bias levels required for the modulator to meet its specifications of carrier suppression, amplitude imbalance, and phase imbalance. The

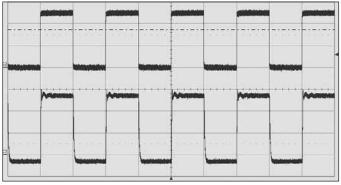
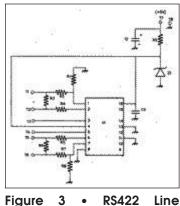


Figure 2 • Input and output of TTL data interface circuit



Receiver circuit

input and output waveforms of the TTL data interface circuit are shown in Fig.2.

RS 422 Interface Circuit

Another logic interface used for data transfer onboard the satellite was RS422. A modulator interface circuit was developed to accept the RS422 levels.

The RS-422 is a differential, or balanced, signaling technique. A termina-

tion resistance of 100 is required at the input of the 422 receiver. The RS422 offers a maximum prescribed common mode voltage range of -7V to +7V, which helps to counter transient spikes and ground shifts.

A twisted pair shielded cable is used for data transmission between the payload and the RF modulator package. At the transmitter end, 26LV31 IC is used. The interface circuit consists of a line receiver and level converter. The line receiver (26LV32) shown in Fig.3 converts RS422 levels to TTL levels. The data is converted to bipolar levels using the level converter shown in Fig.4. The potentiometers are tuned to get bipolar levels which are suitable for biasing the modulator. The differential inputs and the bipolar output of the RS422 data interface circuit is shown in Fig.5.

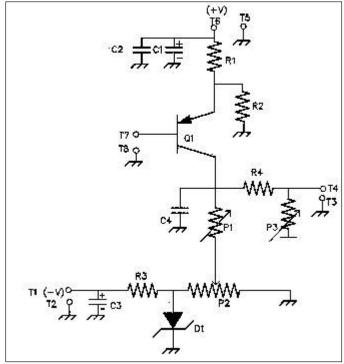


Figure 4 • Level converter in the RS422 driver interface circuit

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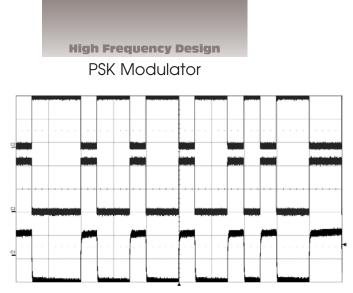


Figure 5 • Differential inputs and output of RS422 interface circuit

Low Voltage Differential Signaling (LVDS) Interface Circuit

The latest interface level currently being used on-board satellite is Low Voltage Differential Signaling (LVDS). An LVDS transmitter (90LV31) converts the processed data into a low voltage differential signal. This is received at the modulator input through twisted pair differential cable. The data interface circuit shown in Fig.6 consists of an LVDS receiver (90LV32) that translates the differential signal into a TTL/CMOS signal. The LVDS receiver has simple termination requirements – usually one resistor at the input of the receiver compared to multiple resistor solutions for other standards. The characteristic impedance of the PCB trace or cable should match with the termination resistor of 100Ω which in turn should be placed as close as possible to the input of the receiver. A 100Ω twisted pair differential cable is used to carry data from the data processing circuits to the modulator.

The output of the LVDS receiver is fed to a latch (54F74) for latching the I and Q data with respect to the clock. This is required to synchronize both the data streams. The clock input to the circuit and the latch can be avoided provided exact length of cables is maintained between the LVDS transmitter and receiver. Also, there should be no skew between the differential pair of lines on the PCB. The latch is followed by a level converter circuit.

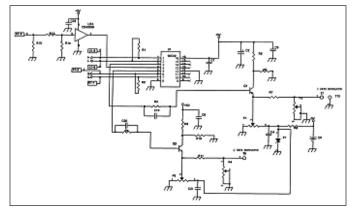


Figure 6 • LVDS driver interface circuit

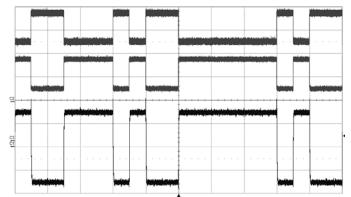


Figure 7 • Differential inputs and output of LVDS driver interface circuit

Potentiometers in the circuit are used to provide suitable bias levels to the modulator. The differential inputs and the output of the LVDS driver interface circuit are shown in Fig.7.

Conclusion

This article discusses various data interface circuits which are practically realized for PSK-based payload data transmission from space to ground. The modulator requires an interface circuit to convert data from different logic levels to the bipolar levels. Data interface circuits such as TTL, RS422 and LVDS are discussed and hardware test results are presented.

About the Authors

Jolie.R received her B.Tech from University of Kerala and M.Tech from Cochin University of Science and Technology. She joined ISRO Satellite Centre, Bangalore in 2000 and is a design engineer for data transmitting systems for IRS satellites. Her work includes development of high bit rate modulators, data transmitters at X and Ka-band and investigations into spectrally efficient data transmission systems for space communication links. She is currently registered for a PhD (part time) at VTU, Bangalore. jolier@isac.gov.in.

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Frequency

Comprehensible Electromagnetics for Comprehensive Engineering

By W. Scott Bennett, Ph.D.

Dr. W. Scott Bennett derives a nanoscale approach to describe the strengths of magnetic and electric near fields that offers an accurate alternative to traditional Hertzian doublet calculations. Electromagnetic theory has long been based on abstract mathematics; however, to be well-engineered, physical causes and effects must be well understood. That has inspired the cause-based explanations of electromagnetic fields that follow.

Charged Particle Fields

One microscopic particle with an electric charge of q (Coulombs) in an otherwise empty medium causes the *r*-directed electric field E_{lr} (Volts/meter).



 Z_m (Ohms) is the *characteristic impedance* of the medium containing q;

 v_p (meters/second) is the *field propagation* velocity in that medium;

r (meters) is the *distance from q to the observation point of* E_{lr} (V/m); and

 $4\pi r^2$ is an *imaginary sphere* in which *q* is centered and on which E_{ir} is observed.

If q moves with a constant velocity of v (meters/second), then qv adds to E_{Ir} (V/m) the ϕ -directed magnetic field H_{ϕ} (Amperes/meter).



An electric dipole is two particles of charge +q and -q separated by a distance $d\ell \rightarrow 0$. And, at any distance $r >> d\ell$ measured from the midpoint of $d\ell$, the charges +q and -q together cause the electric fields E_{2r} and $E_{2\theta}$ (V/m).



These expressions for E_{2r} and $E_{2\theta}$ result, because $d\ell \rightarrow 0$ and $r >> d\ell$ for almost all *r*. And, when $r >> d\ell$, the propagation distances from $\pm q$ to (r, θ, ϕ) effectively equal

 $r \mp \cos\theta d\ell/2$. So, the added electric fields of +q and -q can be accurately viewed as

$$E_{2r} = \frac{r^2 E_{1r}}{\left(r - \frac{\cos\theta dt}{2}\right)^2} - \frac{r^2 E_{1r}}{\left(r + \frac{\cos\theta dt}{2}\right)^2} = \frac{\left(r + \frac{\cos\theta dt}{2}\right)^2 - \left(r - \frac{\cos\theta dt}{2}\right)^2}{\left(r^2 - \left(\frac{\cos\theta dt}{2}\right)^2\right)^2} r^2 E_{1r} = \frac{2\cos\theta dt}{r} E_{1r} \quad (V/m)$$

and

1

$$E_{2\theta} = \frac{\frac{\sin\theta d\ell/2}{r - \frac{\cos\theta dt}{2}} E_{1r} + \frac{\frac{\sin\theta d\ell/2}{r + \frac{\cos\theta dt}{2}} E_{1r}}{r + \frac{\cos\theta dt}{2}}$$
$$= \frac{\left(r + \frac{\cos\theta dt}{2}\right) + \left(r - \frac{\cos\theta dt}{2}\right)}{r^2 - \left(\frac{\cos\theta dt}{2}\right)^2} \frac{\sin\theta d\ell}{2} = \frac{\sin\theta d\ell}{r} E_{1r} \quad (V/m)$$

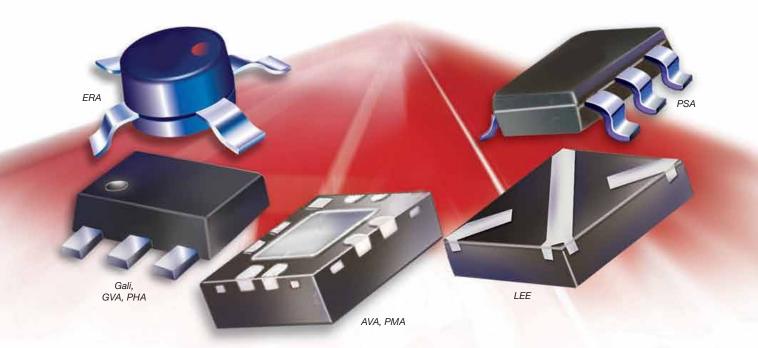
because

$$\left(\frac{\cos\theta d\ell}{2}\right)^2 \leq \left(\frac{d\ell}{2}\right)^2$$
 and $\left(\frac{d\ell}{2}\right)^2 \cong 0$

Point Source Fields

A stationary volume dV containing numerous microscopic particles that have a net electric charge of Q (C) causes the electric field E_{lr} (V/m).

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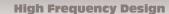
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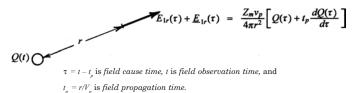
IF/RF MICROWAVE COMPONENTS



Electromagnetic Theory



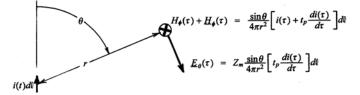
A time-varying net charge of Q(t) (C) in dV will cause the two-component electric field $E_{\mu}(\tau) + E_{\mu}(\tau)$ (V/m).



If some of the particles in dV are moving in the direction of its length dl, a steady movement of net charge, Idl (Axm), causes the magnetic field H_{\bullet} (A/m).



A time-varying charge movement $i(t)d\ell$ (Axm) causes the two-component magnetic field $H_{\phi}(\tau) + \underline{H}_{\phi}(\tau)$ (A/m) and the electric field $\underline{E}_{\theta}(\tau) = Z_m H_{\phi}(\tau) (V/m)$



A <u>nanocurrent $i(t)d\ell$ </u> is a volume dV of length $d\ell$ and cross-sectional area dA, that contains both the moving *charge* $i(t)d\ell$ (Axm), and the *net charge*

$$Q(t) = \int_{0}^{t} (i_{in}(t) - i_{out}(t))dt = d\ell \int \frac{di(t)}{d\ell} dt$$
$$= \frac{d\ell}{v_{pc}} \int di(t) = \frac{i(t)d\ell}{v_{pc}}$$
(C)

where $v_{pc} = dt/dt$ (m/s) is the field propagation velocity in dV.

Therefore, a nanocurrent i(t)dt has the point-source fields

$$H_{\phi}(\tau) + H_{\phi}(\tau) = \frac{\sin\theta}{4\pi\tau^2} \left[i(\tau) + t_p \frac{di(\tau)}{d\tau} \right] d\ell \tag{A/m}$$

$$\underline{E}_{\theta}(\tau) = Z_m \frac{\sin\theta}{4\pi r^2} \left[t_p \frac{di(\tau)}{d\tau} \right] d\ell \qquad (V/m)$$

$$\frac{E}{\theta}(\tau) = Z_m \frac{\sin(\tau)}{4\pi r^2} \left[t_p \frac{\sin(\tau)}{d\tau} \right] d\ell \qquad (V/m)$$

$$E_r(\tau) + \underline{E}_r(\tau) = \frac{Z_m v_p}{4\pi r^2} \left[i(\tau) + t_p \frac{di(\tau)}{d\tau} \right] \frac{d\ell}{v_{pc}} \qquad (V/m)$$

 $E_r(\tau) + \underline{E}_r(\tau)$ $H_{\phi}(\tau) + H_{\phi}(\tau)$ $_{\theta}(\tau)$ i(t)

The Hertzian Dipole and Its Fields

A Hertzian dipole would be two nanocurrents, one that has end-currents of 0 and - i(t), and the other with end-currents of i(t) and 0. So, an isolated Hertzian dipole would have net charges of

$$\int (0 - i(t))dt = -q(t) \text{ and } \int (i(t) - 0)dt = +q(t)$$
 (C)

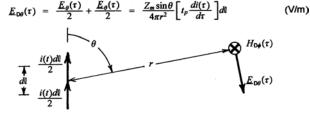
separated by $d\ell$, and the fields of +q(t) and -q(t) would add the same as the fields of +q and -q of an electric dipole, to be

$$E_{\rm Dr}(\tau) = \frac{2\cos\theta d\ell}{r} [E_{\rm 1r}(\tau) + \underline{E}_{\rm 1r}(\tau)] = 2 \frac{Z_m \cos\theta}{4\pi r^2} \left[\frac{q(\tau)}{l_p} + i(\tau) \right] d\ell \qquad (V/m)$$

The fields of moving charge would be those of two adjacent nanocurrents, each with an average current of i(t)/2 and length dl. Therefore, because $dl \to 0$, for all $r >> d\ell$ the fields of moving charge would equal those of one nanocurrent *i(t)dt*.

$$H_{\mathsf{D}\phi}(\tau) = 2\left[\frac{H_{\phi}(\tau)}{2} + \frac{H_{\phi}(\tau)}{2}\right]d\ell = \frac{\sin\theta}{4\pi r^2}\left[i(\tau) + t_p \frac{di(\tau)}{d\tau}\right]d\ell \quad (\mathsf{A/m})$$

and



Thus, an isolated Hertzian dipole's fields would be

$$E_{\rm Dr}(\tau) = \frac{2Z_m \cos\theta}{4\pi r^2} \left[\frac{q(\tau)}{t_p} + i(\tau) \right] d\ell \qquad (V/m)$$

$$H_{\mathsf{D}\phi}(\tau) = \frac{\sin\theta}{4\pi r^2} \left[i(\tau) + t_p \frac{di(\tau)}{d\tau} \right] d\ell \qquad (A/m)$$

and

$$E_{D\theta}(\tau) + \underline{E}_{D\theta}(\tau) = \frac{Z_m \sin\theta}{4\pi r^2} \left[\frac{q(\tau)}{t_p} + i(\tau) + t_p \frac{di(\tau)}{d\tau} \right] d\ell \qquad (V/m)$$

These field equations can be related to textbook equations [1-6] for the fields of a Hertzian dipole, as follows. If μ is the *permeability* of the medium containing i(t)dt, and ϵ is the *permittivity* of that medium, then

$$Z_m = \sqrt{\frac{\mu}{\epsilon}}$$
 (Ohms) and $v_p = \frac{1}{\sqrt{\mu\epsilon}}$ $\left(\frac{\text{meters}}{\text{second}}\right)$

and

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Electromagnetic Theory

And, if i(t) is assumed to be a sinusoidal current, then as in [1], for example, the replacements

$$i(\tau) \leftarrow I_0 e^{j\omega(t-r/c)}, \quad q(\tau) \leftarrow \frac{I_0 e^{j\omega(t-r/c)}}{j\omega}, \quad \frac{di(\tau)}{d\tau} \leftarrow j\omega I_0 e^{j\omega(t-r/c)}$$

and

make

$$dl \leftarrow L$$
, $v_p \leftarrow c$, $t_p \leftarrow \frac{r}{c}$, and $Z_m \leftarrow \frac{1}{\epsilon c}$

$$E_{Dr}(\tau) = Z_m \frac{2\cos\theta}{4\pi r^2} \left[\frac{q(\tau)}{I_p} + i(\tau) \right] d\ell$$

$$= \frac{1}{\epsilon c} \frac{2\cos\theta}{4\pi r^2} \left[\frac{I_0 e^{j\omega r}}{j\omega r/c} + I_0 e^{j\omega r} \right] L$$

$$= \frac{I_0 e^{j\omega (l-r/c)} L \cos\theta}{2\pi \epsilon} \left[\frac{1}{cr^2} + \frac{1}{j\omega r^3} \right] = E_r \qquad (V/m)$$

and

ŀ

$$\begin{aligned} H_{D\phi}(\tau) &= \frac{\sin\theta}{4\pi r^2} \left[i(\tau) + t_p \frac{di(\tau)}{d\tau} \right] d\ell \\ &= \frac{\sin\theta}{4\pi r^2} \left[I_0 e^{j\omega \tau} + \frac{r}{c} j \omega I_0 e^{j\omega \tau} \right] L \\ &= \frac{I_0 e^{j\omega(\tau-r/c)} L \sin\theta}{4\pi} \left[\frac{j\omega}{cr} + \frac{1}{r^2} \right] = H_{\phi} \end{aligned}$$
(A/m)

and

$$\begin{split} E_{\mathsf{D}\theta}(\tau) + \underline{E}_{\mathsf{D}\theta}(\tau) &= Z_m \frac{\sin\theta}{4\pi r^2} \bigg[\frac{q(\tau)}{t_p} + i(\tau) + t_p \frac{di(\tau)}{d\tau} \bigg] d\ell \\ &= \frac{1}{\epsilon c} \frac{\sin\theta}{4\pi r^2} \bigg[\frac{I_0 e^{j\omega \tau}}{j\omega r/c} + I_0 e^{j\omega \tau} + \frac{r}{c} j\omega I_0 e^{j\omega \tau} \bigg] L \\ &= \frac{I_0 e^{j\omega(r-r/c)} L \sin\theta}{4\pi \epsilon} \bigg[\frac{j\omega}{c^2 r} + \frac{1}{cr^2} + \frac{1}{j\omega r^3} \bigg] = E_{\theta} \quad (\mathsf{V}/\mathsf{m}) \end{split}$$

Conclusion

The moving charge *Idt* of a nanocurrent *Idt* causes the magnetic field

$$H_{\phi} = \frac{\sin\theta}{4\pi r^2} I d\ell \tag{A/m}$$

And, the moving charge $Id\ell$ also causes the net charge $Id\ell/v_{n\ell}$, which is the cause of the *electric field*

$$\mathbf{E}_r = \frac{Z_m v_p}{4\pi r^2} \frac{Id\ell}{v_{pc}} \tag{V/m}$$

A time-varying nanocurrent i(t)dt causes the magnetic field

(1)
$$H_{\phi}(\tau) = \frac{\sin\theta}{4\pi r^2} \left[i(\tau) + t_p \frac{di(\tau)}{d\tau} \right] d\ell \qquad (A/m)$$

and the electric field

(2)
$$\boldsymbol{E}_{\theta}(\tau) = Z_m \frac{\sin\theta}{4\pi r^2} \left[t_p \frac{di(\tau)}{d\tau} \right] d\ell \qquad (V/m)$$

Its net charge $i(t)dt/v_{sc}$ causes the electric field

$$\boldsymbol{E}_{r}(\tau) = \frac{Z_{m}k}{4\pi r^{2}} \left[i(\tau) + t_{p} \frac{di(\tau)}{d\tau} \right] d\ell \qquad (V/m)$$

where $k = v_p / v_{pc}$. And, <u>in very many, if not all, important</u> cases k = 1, and

(3)
$$\boldsymbol{E}_{r}(\tau) = \frac{Z_{m}}{4\pi r^{2}} \left[i(\tau) + t_{p} \frac{di(\tau)}{d\tau} \right] d\boldsymbol{\mathbb{V}}$$
(V/m)

The velocities v_p and v_{pc} will be equal when the medium containing i(t)dt is either free space, a vacuum, or air, and the i(t) conductor is copper, lead, aluminum, silver, or gold, for example. That follows, because their relative permeabilities and relative permittivities are all equal to 1.

Based on [1 - 7], on [8], and all of the above – especially on equations (1), (2) and (3) immediately above – it is quite clear that nanocurrents should replace Hertzian dipoles as current elements. The result will undoubtedly be more accurate near-field computations and more comprehensible engineering electromagnetics.

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About the Author

W. Scott Bennett, Ph.D., served as Assistant Professor at Virginia Polytechnic Institute, where he taught electromagnetics and computer design. He later worked at Hewlett-Packard Company where for 16 years he designed computers and made those designs electromagnetically compatible. Since retiring he has worked to rid basic electromagnetics of abstract mathematics and thus make it easier to understand. He can be reached at: w.scottbennett@juno.com.

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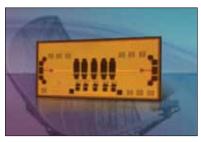
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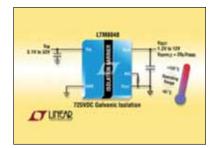
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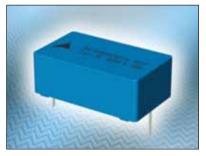
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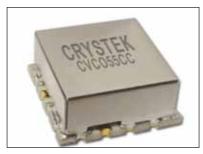
Capacitors

TDK-EPC has developed a wide range of EPCOS MKP and MKT film capacitors with low insertion heights. The new capacitors of the



B32*6T series with a lead spacing of 37.5 mm feature insertion heights of only 15 or 19 mm. These components are designed for rated voltages of between 63 and 2000 V DC or 250 to 400 V AC. Their capacitance ranges from 0.1 to 82 µF. Depending on type and technology (MKT or MKP), these capacitors are designed for maximum operating temperatures of 105, 110 or 125 °C. Applications include DC link circuits as well as DC or AC filtering in converters and power supplies. Their reduced insertion heights make these capacitors especially suitable for applications that require a lowprofile design. These include induction cookers, photovoltaic micro inverters, power supplies for flat-screen TV sets and LED lighting. Thanks to their low insertion heights, they offer very high mechanical resistance to vibrations and shocks, making them equally suitable for subassemblies in automotive electronics.

TDK-EPC epcos.com



VCO

Crystek's CVCO55CC-3750-3800 VCO (Voltage Controlled Oscillator) operates from 3750 MHz to 3800 MHz with a control voltage range of 0.5V~16V. This VCO features a typical phase noise of -105 dBc/Hz @ 10KHz offset and has excellent linearity. Output power is typically +2 dBm. Engineered and manufactured in USA, the model the CVCO55CC-3750-3800 is packaged in the industry-standard 0.5in. x 0.5-in. SMD package. Input voltage is 5V, with a max. current consumption of 30 mA. Pulling and Pushing are minimized to 1.0 MHz and 2.5 MHz/V, respectively. Second harmonic suppression is -15 dBc typical.

Crystek Crystek.com



Beamforming Networks

KRYTAR offers the widest frequency coverage in single-packaged beamforming network designs and provides superior performance in a wide range of RF and microwave applications. KRYTAR's long history of excellence in the design of broadband microwave components including directional couplers, detectors, quadrature hybrids, power dividers/combiners, terminations and coaxial adapters, offers the unique ability to produce ultra-broadband passive beamforming network solutions. RF and microwave system engineers can look to KRYTAR to take the confusion and complexity out of their design challenges with unique mechanical and electrical solutions using proprietary computer-aided-engineering (CAE) tools. KRYTAR beamforming networks are multifaceted assemblies for a wide range of applications including multiple antenna and antenna arrays used in military electronic systems and commercial communications systems.

KRYTAR krytar.com

A high performance signal analyzer ready to take you into the wireless future.



Wireless technology never stops moving forward. Success depends on your ability to evolve. The Agilent PXA signal analyzer helps you keep ahead by maximizing flexibility, scalability and longevity so you can drive your evolution.

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Scan or visit http://goo.gl/c5PjF for videos on optimized signal analysis

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Up to -88 dBc 3GPP ACLR dynamic range

LTE and HSPA+; just two of over 25 measurement apps.

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Agilent Technologies

High Frequency Products

NEW PRODUCTS



Resistors

Vishay Intertechnology, Inc. introduced a new series of dual-in-line thin film resistor networks offering a wide operating temperature range of - 55 °C to + 215 °C. Providing nearly a 100 °C extension in operating temperature range over traditional thin film chip resistors, the HTRN series features low absolute TCR of \pm 25 ppm/°C, TCR tracking of 5 ppm/°C, and tight ratio tolerances to ± 0.05 %. Featuring a rugged, molded 50 mil pitch construction with no internal solder, the HTRN series of resistor networks offers four isolated resistors with a wide resistance range of 1 k to 100 k per resistor, with divider ratios from 2:1 to 100:1. The devices feature very low noise of < - 35 dB, low voltage coefficients of 0.1 ppm/V, and a power rating of 100 mW per element (400 mW per package).

Vishay Intertechnology vishay.com



Filter

Mini-Circuits' new ZX75LP-288+ is a 50 low pass filter built in a connectorized package. Covering DC to 288 MHz bandwidth, these units offer good matching within the passband and high rejection in stopband. This will find its applications in receivers and transmitters to suppress spurious emission and harmonics. It has repeatable performance across production lots and consistent performance across temperature. Features and advantages: Low passband insertion loss: suitable for high performance application; Fast roll-off -- Provides very good adjacent band rejection; Connectorized package: The connectorized package is easy to interface with other devices and well suited for test setups; Good VSWR: Provides good interface when used with other devices.

Mini-Circuits minicircuits.com



LNA

MITEQ Inc. introduces a new addition to its family of high-performance waveguide LNAs. The Model AMFW-7F-17702130-120-23P-WP is a very low noise, high dynamic range weatherproof Ka-band front end, operating 17.7 to 21.3 GHz. With isolator protected and pressure sealed WR-42 waveguide input and K(F) connector output, in addition to being lightweight, this low-noise amplifier has a small profile and footprint. The aluminum alloy housing is sealed against most severe environmental conditions and also fully EMI shielded. This LNA includes reverse voltage, over current and over temperature protection in addition to full internal regulation. Total weight is approximately 800 grams, and dimensions are 156mm x 70mm x 51mm. The AMFW-7F-17702130-120-23P-WP has a minimum gain of 60 dB, flat to within ±1 dB, and maximum noise temperature of 120 K° and is capable of a minimum of 23 dBm P1dB across the full band.

MITEQ, Inc. miteq.com



Switch

PMI Model P2T-18G40G-65-R-292FF is a Single Pole, Two Throw, Solid-State Switch which operates over the 18GHz to 40.0GHz frequency range. This model provides 55dB of isolation over the entire frequency range of operation and offers low insertion loss performance with fast switching speeds. Features: 18GHz to 40GHz Operation; High Isolation; Low Insertion Loss; High Speed; Compact Size.

Planar Monolithics Industries pmi-rf.com



PLL Chip Set

Hittite announced a new market leading PLL chip set. The HMC983LP5E DC to 7 GHz Fractional-N Divider and Frequency Sweeper and the HMC984LP4E Digital Phase-Frequency Detector and Charge Pump form a high performance PLL chip set solution targeted at PLL and Frequency Modulated Continuous Wave (FMCW) sweeper applications requiring ultimate performance. The HMC983LP5E integrates the industry's largest programmable 48-bit Delta-Sigma Modulator which allows the combined PLL to achieve unparalleled fractional frequency resolution of 180 nHz. A built-in frequency sweeper enables the combined PLL to generate identical, coherent, FMCW frequency sweeps that can



0.15-6200 MHz as low as 99 each (qty. 1000) OR ON COMPLIANT.

Rugged, repeatable performance.

At Mini-Circuits, we're passionate about transformers. We even make own transmission line wire under tight manufacturing control, and utilize all-welded connections to maximize performance, reliability, and repeatability. And for signals up to 6 GHz, our rugged LTCC ceramic models feature wraparound terminations for your visual solder inspection, and they are even offered in packages as small as 0805!

Continued innovation: Top Hat.

30. 7761442

A Mini-Circuits exclusive, this new feature is now available on every open-core transformer we sell. Top Hat speeds customer pick-and-place throughput in four distinct ways: (1) faster set-up times, (2) fewer missed components,

(3) better placement accuracy and consistency, and (4) high-visibility markings for quicker visual identification and inspection.

More models, to meet more needs

Mini-Circuits has over 200 different SMT models in stock. So for RF or microwave baluns and transformers, with or without center taps or DC isolation, you can probably find what you need at minicircuits.com. Enter your requirements, and Yoni2, our patented search engine, can identify a match in seconds. And new custom designs are just a phone call away, with surprisingly quick turnaround times gained from over 40 years of manufacturing and design experience!

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212 The Design Engineers Search Engine finds the model you need, Instantly · For detailed performance specs & shopping online see minicircuits.com

High Frequency Products

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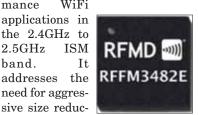
be linear, user-defined, automatic or triggered.

Hittite Microwave Corp. hittite.com

Front End Module

RFMD's new RFFM3482E Front End Module (FEM) is a single-chip integrated FEM for high-performance WiFi

applications in the 2.4GHz to 2.5GHz ISM It band. need for aggressive size reduction for typical



802.11b/g/n front end designs and greatly reduces the number of components outside of the core chipset. RFFM3482E has an integrated b/g/n power amplifier, directional power detector, Rx balun, and Tx filtering. It is also capable of switching between WiFi Rx,

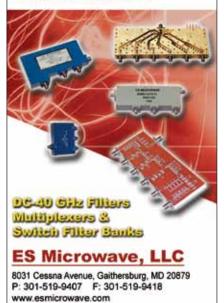
ES MICROWAVE LLC.

Since 1985 we have offered our custom design filters and sub-assemblies in combline, interdigital and suspended-substrate technologies.

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Suspended-Substrate

Filters, Diplexers, Triplexers, Quadruplexers, Quintuplexers, Sextuplexers...



WiFi Tx, and Bluetooth Rx/Tx operations. In a 3 mm x 3 mm x 0.45mm, 16-pin package, this module meets or exceeds the RF front end needs of 802.11b/g/n WiFi RF systems.

RFMD rfmd.com

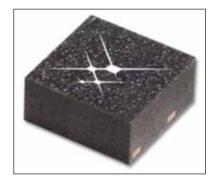




Attenuator

Mini-Circuits' new BW-N6W20+ precision fixed attenuator features: DC to 18 GHz operation; precise attenuation; excellent VSWR of 1:30:1 typical; and stainless steel N male and female connectors. Applications include matching, instrumentation; test set-ups, and high-power measurements. Maximum ratings: operating temperature: - 55 deg C to 100 deg C. Storage temperature: - 55 deg C to 100 deg C. The new BW-N6W20+ is RoHS compliant in accordance with EU Directive (2002/95/EC).

Mini-Circuits minicircuits.com



PIN Diode

Skyworks Solutions has introduced a high power series PIN diode for transmit and receive switching applications. The SMP1325-087LF is a discrete solution available in a high-thermal dissipative package - making it ideal for large signal switching

and attenuation applications. It combines very low-insertion (0.04 dB) loss, high linearity (90 dBm), good isolation, excellent power handling (35W) and low distortion in a very small package. Target markets include handsets, infrastructure, military and others that may require high-power switching.

Skyworks Solutions, Inc. skyworksinc.com



D/A Converters

Analog Devices, Inc. introduced D/A (digital-to-analog) converters that provide high accuracy and ultra-low noise, simplifying the design of precision instrumentation and analytical equipment. The new high-accuracy D/A converters incorporate integrated precision reference conditioning circuitry, making them system ready and providing a 60 percent reduction in board space compared to competing standalone data converters. The high linearity and low noise of the AD5790 and AD5780 D/A converters reduce the need to calibrate systems for nonlinearity or to time-average multiple measurements. The high stability and low drift of the converters over time and temperature reduce the need to compensate systems for aging and temperature effects. These features combine to significantly improve repeatability, reduce system downtime, and lower system maintenance costs.

Analog Devices, Inc. analog.com

LVFR

ON Semiconductor introduced of a new family of 100 volt (V) trenchbased low forward voltage Schottky

You work in all kinds of conditions, so should your spectrum analyzer.





Scan the QR code or visit http://goo.gl/JgXjo to see a HSA N93442 demo guide video Only Agilent analyzers give you benchtop performance in a lightweight MIL-PRF 28800F Class 2-compliant handheld. Including a rugged design with no fans and no vents for tough field environments. So even in worstcase conditions, you can perform at your peak.

That's thinking ahead. That's Agilent.

Handheld Spectrum Analyzers (HSA)

Key Specs	N9344C	N9343C	N9342C	N9340B
Frequency	1 MHz– 20 GHz	1 MHz– 13.6 GHz	100 kHz– 7 GHz	100 kHz– 3 GHz
DANL	-155 dBm/Hz	-155 dBm/Hz	-164 dBm/Hz	-164 dBm/Hz
Sweep time	< 0.9 s	< 0.7 s	< 0.4 s	< 0.1 s
Weight with battery	3.6 kg (7.9 lbs)	3.6 kg (7.9 lbs)	3.6 kg (7.9 lbs)	3.5 kg (7.7 lbs)

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High Frequency Products

NEW PRODUCTS



rectifiers (LVFR) for applications such as switching power supplies for notebook adapters or flat panel displays, reverse battery protection circuits, and high frequency DC-DC converters. The new NTST30100CTG, NTST20100CTG and NTSB20U100CTG family of devices utilize a trench topology that enables exceptionally low forward voltage drop and reduced leakage current. This results in low conduction losses and a substantial improvement in circuit efficiency, helping design engineers achieve regulatory requirements without the added complexity, such as synchronous rectification

ON Semiconductor onsemi.com

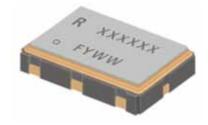


Sensor

API Technologies Corp. announced a new output option for its Spectrum Sensors line of H009 Hall Effect Position Sensors. The new 4-20mA output option joins the existing H009 series with Analog, PWR, and Serial output options. Hall Effect Position Sensors convert relative changes in a magnetic field into an electrical signal to provide position change information. Hall Effect Position Sensors are used in a variety of applications in the medical, wind measurement, green energy, robotics, and military and

aerospace markets. The API Spectrum Sensors H009 Hall Effect Series are .875 inch in diameter with a .750 maximum length. They have a 12-bit resolution with a rotational life of over 100 million revolutions and feature an absolute linearity of +/- 0.1% at room ambient and +/- 0.3% at -40° to +125°C. They are available with several options including: lead wires, lead lengths and terminations; HR370 High TG printed circuit boards; and JST and Molex terminals. Special shaft, flange mounting, and gear mounting frame configurations are also available.

API Technologies Corp. apitechnologies.com



VCXO

Rakon announced a new family of low noise, frequency selectable XO (RXO7050Q) and VCXO (RVX7050Q) products in industry standard 7 mm x 5 mm surface mount packages. The frequency select pins are used to select the output frequency from any combination of two or four pre-configured frequencies. The selectable capability increases design flexibility and reduces part count, to generate significant cost savings. The RXO7050Q and RVX7050Q deliver a frequency output from 8 MHz to 1.5 GHz with <1 ps RMS phase jitter (integrated 12 kHz to 20 MHz), to address high speed serial data communications, networking and telecom applications. The Q Series offer a low cost, pincompatible alternative to SiLabs proprietary Si5xx selectable oscillators. Smaller footprints are available soon.

Rakon rakon.com



ASR

- VNA Test Port Assembly
- Durable Connector Designs
- Maintains Test Configuration
- Low-Loss Cable Construction
- Phase-Matched Pairs Available

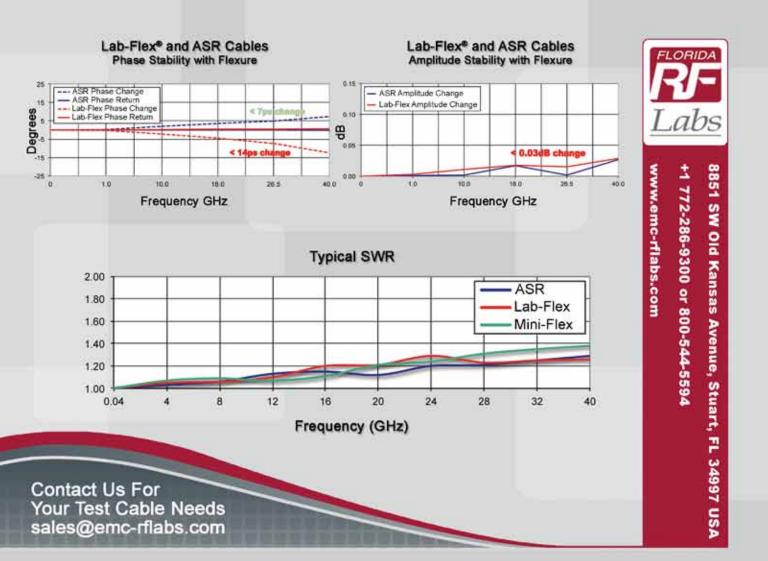
Lab-Flex®

- Great General Purpose Test Assembly
- Low-Loss Construction
- 90dB Minimum Shielding
- Superior Connector Designs
 Excellent Strain Relief / Extended Boots

Mini-Flex & RG Cables

- Cost-Effective Test Assemblies
- · Wide Variety of Connector Options
 - Stainless Steel Connector Designs
 - · Up to 90dB Minimum Shielding
 - Protective Coverings Available

All cable groups offer performance up to 50 GHz





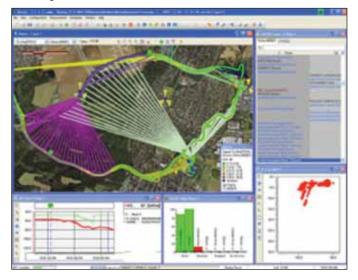
Universal Radio Network Analyzer

The R&S®TSMW universal radio network analyzer is a high-end platform for optimizing all conventional wireless communications networks. Two highly sensitive 20 MHz frontends for any input frequency from 30 MHz to 6 GHz, a dual-channel preselection and an FPGA-



based software-defined architecture offer unsurpassed performance while providing maximum flexibility and operational readiness. In addition to functioning as a scanner for wireless communications networks in combination with theR&S@ROMES4 drive test software, the R&S@TSMW is also an ideal digital I/Q baseband receiver for customer-specific applications.

- User-definable input frequency range from 30 MHz to 6 GHz
- Two independent RF and signal processing paths, each with a bandwidth of 20 MHz
- Integrated preselection for high intermodulation suppression while dynamic range is high
- Support of LTE FDD and TD-LTE measurements together with the R&S®ROMES4 drive test software
- Parallel measurements in GSM, WCDMA, LTE, cdma2000®1xEV-DO, TETRA and WiMAX[™] networks
- Spectrum measurements with the RF power scan option





- I/Q baseband streaming with Gigabit LAN interface to a PC or via R&S®digital I/Q interface to the R&S®IQR I/Q data recorder
- Integrated GPS with PPS

Drive Test Software

R&S®ROMES4 is a test platform for measurements in all mobile radio networks. In combination with R&S®TSMx network scanners and test mobile phones, it forms a complete system for coverage and quality of service (QoS) measurements. Besides pure recording and visualization of test parameters, data is processed instantly and statistics are calculated in realtime.

One software solution for all technologies: "all under one roof"

Flexible handling of software licenses reduces startup costs

Parallel measurement with up to 16 mobile phones per license; this saves time, allowing existing resources to be utilized more effectively: reduction of operating expenses (OPEX)

Use of highly accurate, fast RF test and measurement equipment (Rohde & Schwarz scanners):

many reliable measured values and results

Numerous advanced features for network troubleshooting

Automatic evaluation after completion of measurement by means of the integrated replay function or theR&S®ROMES4NPA (network problem analyzer), which considerably reduces OPEX

Automatic identification of GSM interferences: considerable OPEX reduction (up to 80 % potential savings compared with standard analysis)

Unique Scanner for LTE and TETRA networks in all bands and decoding of broadcast information

Rohde & Schwarz Rohde-schwarz.com

Product Showcase





In business since 1988, Special Hermetic Products, Inc. has been a leader in the hermetic seal business for over 20 years. In addition to hermetic feedthrus, capacitors, connectors, headers and related products & services, SHP offers solutions for all your custom hermetic design requirements. SHP is ISO 9001:2008 Certified.



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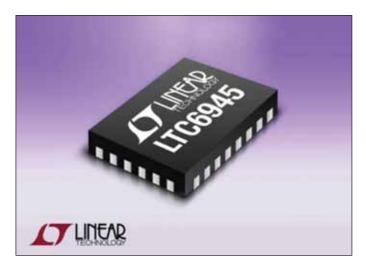
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www.highfrequencyelectronics.com

PRODUCT HIGHLIGHT



14-Bit A/D Converters

The LTC®2145-14/LTC2144-14/LTC2143-14 are 2-channel simultaneous sampling 14-bit A/D converters

designed for digitizing high frequency, wide dynamic range signals. They are perfect for demanding communications applications with AC performance that includes 73.1dB SNR and 90dB spurious free dynamic range (SFDR).

Ultralow jitter of 0.08psRMS allows undersampling of IF frequencies with excellent noise performance.

DC specs include $\pm 1LSB$ INL (typ), $\pm 0.3LSB$ DNL (typ) and no missing codes over temperature. The transition noise is 1.2LSBRMS.

The digital outputs can be either full rate CMOS, double data rate CMOS, or double data rate LVDS. A separate output power supply allows the CMOS output swing to range from 1.2V to 1.8V.

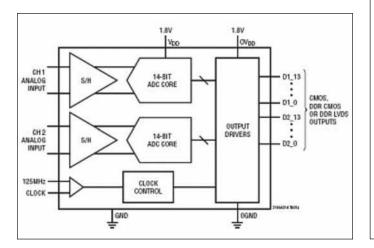
The ENC+ and ENC- inputs may be driven differentially or single-ended with a sine wave, PECL, LVDS, TTL, or CMOS inputs. An optional clock duty cycle stabilizer allows high performance at full speed for a wide range of clock duty cycles.

Integer-N PLL/Synthesizer

Linear Technology announces the LTC6945, a high performance 6GHz integer-N frequency synthesizer with outstanding -226dBc/Hz normalized closed-loop in-band phase noise, excellent -274dBc/Hz normalized in-band 1/f noise, a wideband phase noise floor of -157dBc/Hz and best-in-class -102dBc spurious output.

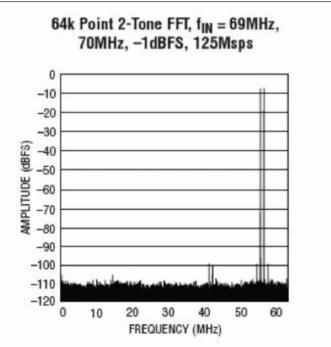
In a typical 900MHz application, these performance attributes enable a closed-loop phase noise of -100dBc/Hz at 1kHz offset. The LTC6945 is designed to work in conjunction with an external low noise VCO up to 6GHz. In addition, the device has an on-chip output divider that is programmable from 1 through 6 to extend the tuning frequency coverage to as low as 350MHz.

The LTC6945 comprises a low noise reference buffer, a reference divider, phase-frequency detector (PFD) with



phase-locked indicator, an ultralow noise programmable charge pump and an integer feedback divider to attain very low noise PLL operation. The on-chip SPI-compatible bidirectional serial port allows frequency tuning and control, and read back of the register and loop status information.

Linear Technology linear.com



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2.4mm	DC-50 GHz		DC-34 GHz	SSMA	DC-40 GHz

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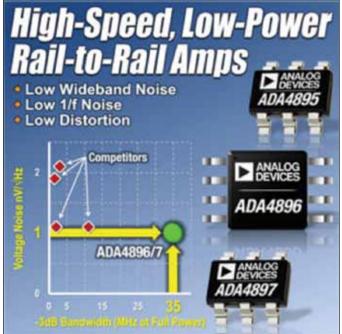


Sensor

Analog Devices released the third generation iSensor® MEMS IMU (inertial measurement unit). The ADIS16488 is a tactical grade 10-degree-of-freedom (DoF) sensor and integrates a tri-axis gyroscope, tri-axis accelerometer, tri-axis magnetometer and a pressure sensor into a single package.

This new MEMS IMU provides the most stable and complete integrated sensor suite available, supporting mission critical requirements in high-performance navigation and stabilization applications. Beyond the important tactical grade (below 10°/hr) bias stability, the ADIS16488 outperforms all other contemporary gyro/ IMU offerings on the often more critical specifications of g-effect, temperature coefficient, and bandwidth by up to 100X. Further, the new iSensor MEMS IMU even outperforms legacy military grade IMUs on vibration rectification and linearity. Every device undergoes unique and extensive factory calibration, resulting in unparalleled precision in the toughest environments and greatly reduces complexity, time, cost, and design risk relative to typical motion sensor development.

The ADIS16488 iSensor 10-DoF MEMS IMU is a complete inertial measurement system that combines ADI's high performance iMEMS® technology and sensor-signal processing expertise to optimize the IMU's 10-DoF dynamic performance. Operation is fully autonomous, including all embedded compensations, with valid data available from the SPI interface 500 ms after applying power. With all calibration done at the factory, and with an ADI Blackfin® processor-powered configurable inter-



face for tuning embedded filtering and other diagnostics, a major source of design integration time and risk is virtually eliminated.

High-Speed Amplifiers

Analog Devices unveiled a series of high-speed amplifiers that establish a new performance standard with the best combination of high-speed, low noise and low power. Designed for portable, multi-channel and low power instrumentation and healthcare equipment, the ADA4896-2 (dual), ADA4897-1(single) and ADA4897-2 (dual) highspeed amplifiers provide the highest large-signal bandwidth and slew rate with the lowest noise available today in a rail-to-rail amplifier under 10 mW.

Each amplifier features low noise of 1 nV/ $\sqrt{\text{Hz}}$ and 120-V/ μ s slew rate while consuming only 3 mA of supply current. Further, the 1/f noise @10Hz is a low 2.4 nV/ $\sqrt{\text{Hz}}$. Watch this video and learn more about ADI's new series of high-speed amplifiers.

Also announced as part of this high-speed amplifier series was the ADA4895-2 dual de-compensated highspeed amplifier. It delivers 1.5-GHz gain-bandwidth product at gains of +10 and greater, making it ideal as a highspeed, high-gain pre-amplifier.

The new rail-to-rail amplifiers operate across the extended industrial temperature range of -40° C to $+125^{\circ}$ C and offer a 3-V to 10-V supply range. The ADA4895-2 and ADA4897-1/ -2 include an output disable feature.

Analog Devices analog.com

High Quality. Higher Freque

Our new high performance series of microwave and millimeterwave connectors can provide you with the benefit of legendary Delta quality over a broad spectrum of frequency and bandwidth requirements.

In addition to our extended-frequency 26.5-GHz SMA connectors, we now offer ultra-precision SMAs with superb performance to 27 GHz, plus 2.92 mm (SMK) connectors to meet your SMA-compatible requirements to 40 GHz, and 2.4 mm production grade connectors that will satisfy your require-ments all the way to 50 GHz. For high-frequency applications requiring minimum connector size or blind mating, our SMP connectors are ideal.

Our new product lines include cable plugs and jacks, and field-replaceable receptacles for use with hermetic seals. These receptacles are available in all common mounting flange and pin size configurations.

Delta's new connectors are designed using state of-the-art optimization tools and techniques. This focus on precision produces connectors with low VSWR, minimal transmission loss, and low RF leakage.

> SOMWBA т

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Call or visit our website to see how Delta Quality RF, microwave, and and millimeterwave connectors can help you meet your product performance goals—from DC to 50 GHz.

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DeltaRF.com

PRODUCT HIGHLIGHT



Electrical-Thermal MMIC Design Flow

AWR Corp. recently authored a useful white paper, "Turn Up the Heat! AWR Connected: An Electrical-Thermal Design Flow."

Excerpt:

"Electronic circuit design typically begins with an assumption that the components are operating at ambient temperature. Monolithic Microwave Integrated Circuit (MMIC) design, in particular, violates this as the DC current flowing through the ever-shrinking devices induces heating to two, three, or even four times greater temperature (in deg C). Such a large departure from assumed room temperature behavior impacts phase, gain, efficiency, noise, and intermodulation distortion. Circuit designers need tools with integrated electrical-thermal analysis to address these performance issues."

Read the entire paper at: http://web.awrcorp.com/content/Downloads/MMIC-Flow-WP.pdf?from=771266750304385

Modelithics Latest Release for AWR Microwave Office

Modelithics, Inc. (www.modelithics.com) has released the latest version of their popular linear and non-linear system level model libraries for RF, microwave and millimeter-wave device and components. The Modelithics COMPLETE Library version 8.0 for AWR's Microwave Office[™] software introduces forty-six (46) new Global Models for passive RLC's, and eighteen (18) new non-linear models for diodes, switches, amplifiers, and transistors.

Nearly all of the existing models for use with AWR's Microwave Office software have been updated with significant enhancements to enable full compatibility with AWR's APLAC® non-linear circuit simulation technology. Version 8.0 also introduces a new measurement-derived

substrate library. The enhanced APLAC compatibility as well as the new Substrate Library were added in response to designer requests to improve the convenience, accuracy and flexibility of their AWR simulations with Modelithics' models.

Designers can download our free model library, Modelithics SELECTTM from www.modelithics.com and see for themselves why designers around the globe consider Modelithics libraries a necessary part of their RF design toolkit. For more information or to request a free full-version trial of the Modelithics COMPLETE Library, send an email to Sales@Modelithics.com , or click on the free trial link you'll find at: http://www.modelithics.com.

AWR awrcorp.com

When failure is not an option.

Johnson's line of SMP connectors are manufactured to MIL-Spec interface standards with consistent quality and performance levels you can depend on in your designs and applications.

Key benefits of using an SMP connector are:

- · Use blind-mate applications
- Micro-miniature slide-on/snap-on interconnect system
- · Bullet design that provides a flexible link between shroud connections
- · Available in custom configurations

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Design Notes & Market Reports

Design Notes

Applied Wave Research (awrcorp.com):

Analog Office Configure

This project will help new users to Analog Office configure the software for some settings that they will be more familiar with. These include the schematic and layout colors, the hotkeys, schematic wires behavior, units, and layout face defaults. This project will also discuss a method to generate a library of elements defined by the user.

Analog Office Extends HSPICE Transient Simulations to RF

Microwave Office, the Applied Wave Research (AWR) product for RF, microwave and millimeter-wave design, offers harmonic balance simulations to obtain steady state waveforms for port voltages and currents in microwave circuits. Design of many types of circuits such as oscillators, frequency dividers, and digital circuits with memory requires the ability to perform transient simulations. AWR's Analog Office (AO) offers this capability for RF and microwave circuits through integration with HSPICE 2003 from Synopsys...

BJT Amp Complete

This example is a part of AO Getting Started Guide.

BJT Amp OpPnt

This project shows the preliminary design of a differential amplifier, in order to demonstrate the DC operating point annotation and measurement in MWOffice and Analog Office.

CustomSpirals

It is easy to create your own custom spiral inductors within the AWR environment. The following simple steps show how to create the spiral element, characterise it and then use it in your project.

HierarchyResExample

The unified database used in the AWRDE contains much more connectivity information than other IC design tools normally would. In order to make the most of the advanced features of Analog Office, hierarchical connection in layout needs to be considered a little differently.

Agilent Technologies: (agilent.com/find/powerofx)

Agilent Technologies has made available a new Application Note on Testing DigRF Interfaces. The new "Solutions for Testing DigRF Interfaces" 5990-9501EN, offers insight into how to quickly and efficiently characterize digital wireless devices. It is part of a series of Agilent Power of X application notes created to provide insight into solving tough measurement problems in a unique way for both the design and manufacturing environments. To request copies of the free application notes go to www.agilent.com/find/powerofx.

MARKET REPORTS

Test Equipment Market in Russia and the CIS

Russia and the CIS countries are emerging markets offering long-term potential for general purpose test equipment vendors. Government and private investments in infrastructure development and services are poised to generate new opportunities for test equipment vendors.

New analysis from Frost & Sullivan (http://www.testandmeasurement.frost.com), General Purpose Test Equipment Markets in Russia and CIS Countries, finds that the markets earned revenue of \$194.8 million in 2010 and estimates this to reach \$247.3 million in 2015. The research service covers the following products: oscilloscopes, signal generators, spectrum analysers, multimeters, network analysers, logic analysers, power meters, arbitrary waveform generators and electronic counters.

"Investments in infrastructure are rising with constant upgrades and efforts at modernisation," notes Frost & Sullivan Industry Manager Sujan Sami. "The increase in public-private partnerships (PPP) is set to boost infrastructure development, leading to greater demand for suitable test equipment."

The education as well as the aerospace and defence (A&D) sectors are major revenue-generating streams in Russia and the CIS countries. The A&D end-user sector was not as badly affected by the economic downturn as other sectors. This, in addition to the growth in the educational sector, is driving demand for oscilloscopes and other general purpose test equipment.

A large territory and customer base also bodes well for market prospects. "Russia is the largest country in the world and is also the 9th largest country in terms of population," explains Sami. "This implies a huge consumer base for electronic products that will attract electronic OEMs and create potential for general purpose test equipment vendors."

At the same time, growth in several industrial sectors is poised to augment demand for general purpose test equipment in the near future. In addition, with the economy recovering from the recession, the pent-up demand

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Design Notes & Market Reports

for general purpose test equipment is set to hit the market, resulting in heightened demand levels.

However, the lack of private capital expenditure threatens to restrain market growth. Poorer economies such as Tajikistan, Armenia, Uzbekistan, Kyrgyzstan and Moldova are mostly dependent on state expenditure for growth. This restricts the adoption of newer technologies, hindering market expansion.

With government policies playing a critical role in the development of countries in the CIS region and in Russia, companies also need to keep a close track of evolving government regulations.

"Focusing on total solutions, rather than just selling test instruments, is the key to achieving market success," concludes Sami. "Moreover, to compete more effectively against regional vendors, companies will need to forge alliances with local channel partners."

If you are interested in more information on this study, please send an email with your contact details to Anna Zanchi, Corporate Communications, at anna.zanchi@frost.com.

"Wireless Decade" for Latin America

Currently, the Latin American region is characterized by the coexistence of 2G, 3G and 4G wireless standards. The lack of standardization has restrained vendors in terms of product development and customer base expansion. However, the future looks bright as regulatory bodies begin playing an important role in aligning with international standards.

New analysis from Frost & Sullivan estimates the markets to expand from \$ 158.5 million in 2010 to \$342.0 million in 2017, growing at a compound annual growth rate (CAGR) of 11.6 percent during the forecast period.

"A key factor driving demand for wireless test equipment is the continuous development of wireless communication standards from 2 and 2.5G to 3G, 3.5G, HSPA and 4G," notes Frost & Sullivan Research Analyst Mariano Kimbara. "There are several 4G trials and deployments slated to begin by the end of 2011 and the beginning of 2012 which are expected to generate growth for this market."

The evolution from 2G to 3G wireless standards has contributed significantly to the uptake of wireless test and equipment in the Latin American region. Operators in Latin America are in the initial phase of 3G HSPA deployments and very few are introducing HSPA +. The new HSPA technologies allow increased data transmission in the region without the need for massive investment. Imminent LTE deployments also augur well for market prospects.

"The major reason for deploying LTE in the region is the promise of reduced operating costs and savings in terms of frequency spectrums over the long term," explains Kimbara. "As a result, operators are favoring the implementation of LTE, instead of blindly following the parameters of developed markets such as those in North America and Europe."

A key challenge is the lack of emphasis on quality, which has had a ripple effect on investment levels. Latin American operators are cost conscious, exhibiting an 'essentials only' attitude towards test equipment. Consequently, vendors are experiencing difficulties in penetrating the market with high-end sophisticated testing tools.

"Regulatory bodies have not been very proactive in auditing network quality," elaborates Kimbara.

"They have shirked from applying penalties in cases where operators have failed to meet the contractually agreed performance in terms of efficiency and quality."

However, things are changing. The explosion of wireless data usage brought about by smartphones has put immense strain on networks in the Latin American region in terms of quality. Regulatory bodies are starting to push for higher quality standards in some countries.

"The rising number of smartphones and tablets sales, combined with high mobile penetration rates, has intensified the need to deploy HSPA+ in large cities," concludes Kimbara. "This will highlight the need for more robust and reliable wireless test and equipment."



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International Microwave Symposium IEEE 17-22 June 2012, Montréal, Canada MTT-S http://ims2012.mtt.org/



IMS2012: Microwaves without Borders



S2012

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The IEEE Microwave Theory and Techniques Society's 2012 International Microwave Symposium (IMS2012) will be held on 17-22 June in Montréal, Canada as the centerpiece of Microwave Week. IMS2012 offers technical sessions, interactive forums, plenary and panel sessions, workshops, short courses, industrial exhibits, application seminars, historical exhibits, and a wide array of other technical and social activities including a guest program. Colocated with IMS2012 are the RFIC symposium (www.rfic2012.org) and the ARFTG conference (www.arftg.org), which comprise the Microwave Week 2012 technical program. With over 9,000 attendees and over 800 industrial exhibits of the latest state-of-the-art microwave products, Microwave Week is the world's largest gathering of Radio Frequency (RF) and microwave professionals and the most important forum for the latest and most advanced research in the area.

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GaN FET PA Design Examples:

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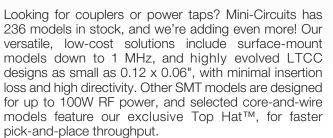


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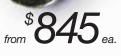


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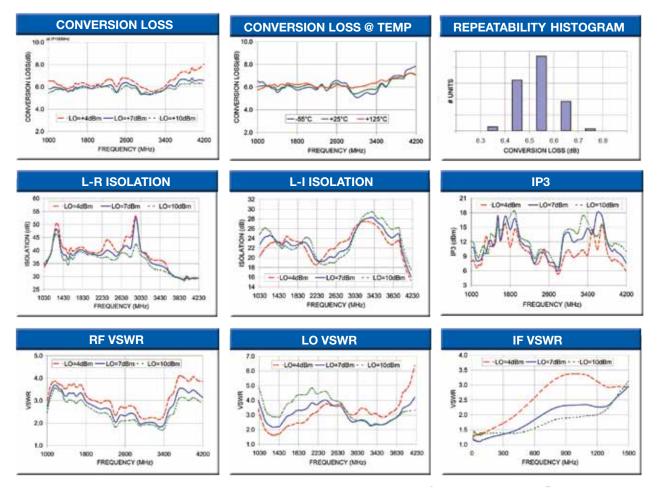
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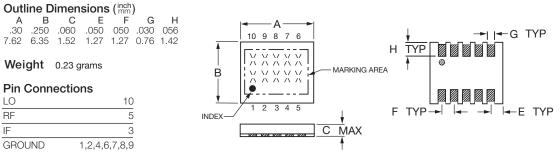
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